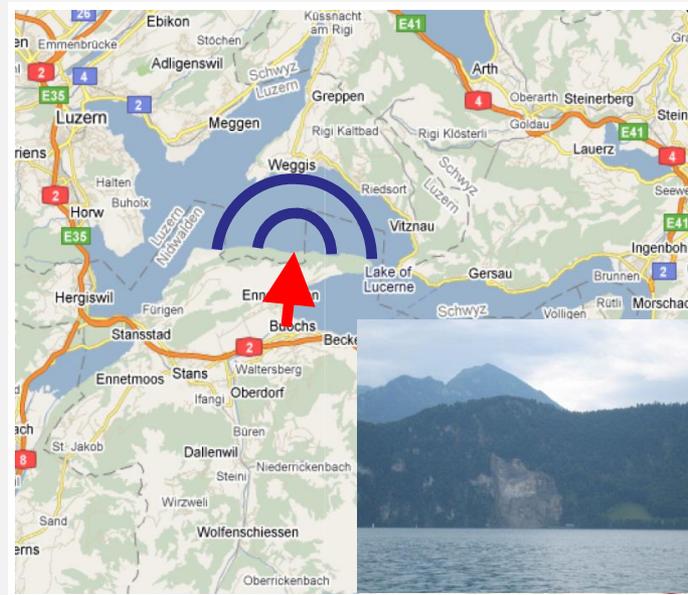


A laboratory-DualSPHysics modelling approach to support landslide-tsunami hazard assessment



Lake Lucerne case,
Switzerland, 2007

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Table of content

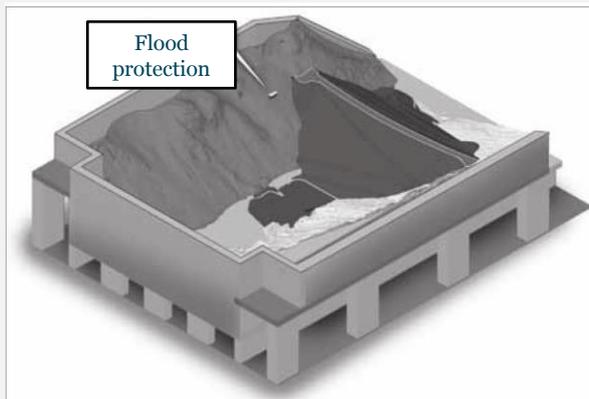
- Introduction
- Models
 - Physical
 - DualSPHysics
- Results
- Conclusions
- Outlook



Introduction

3 main methods to predict landslide-tsunamis (impulse waves)

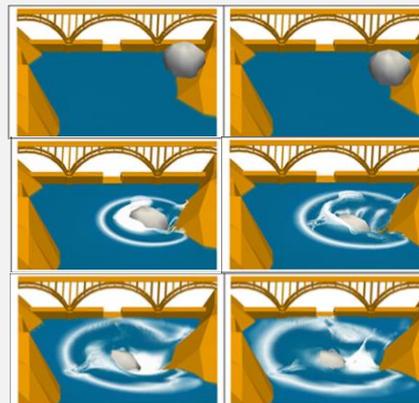
(i) Case-specific physical modelling



Küthai reservoir at 1:130 (Fuchs et al. 2011)

- + Most accurate
- Time consuming and expensive (> 1 year)

(ii) Case-specific numerical modelling



SPH model (Gomez-Gesteira et al. 2012)

- +/- Reasonable accurate
- +/- Time consuming/expensive (weeks - months)

(iii) Generic empirical equations based on idealised conditions



Tests of present study in wave basin

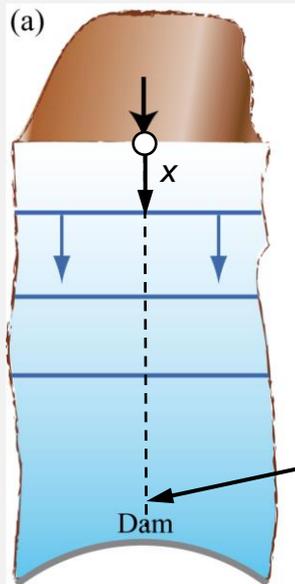
E.g. $a_{M,2D} = (4/9)P^{4/5}h$ (Heller & Hager 2010)

- Delivers estimates only
- + Efficient, inexpensive and fast (days)

Introduction

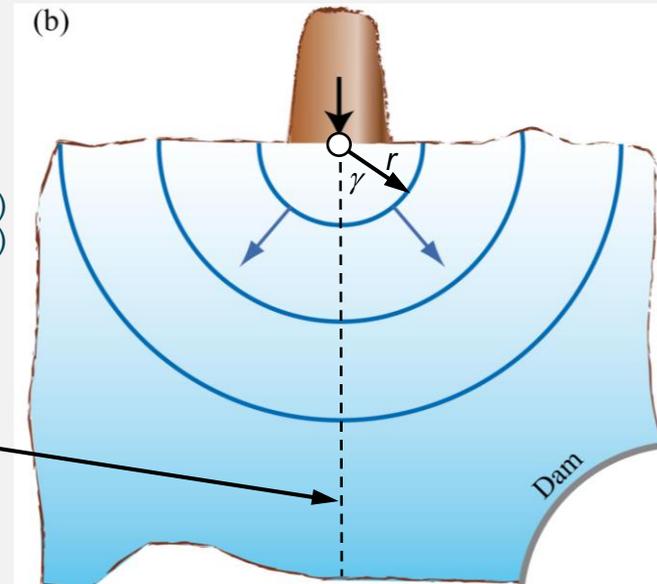
Idealisation of the water body geometry: 2D versus 3D

2D: Wave flume geometry



x = streamwise distance (2D)
 r = radial distance (3D)
 γ = wave propagation angle (3D)

3D: Wave basin geometry

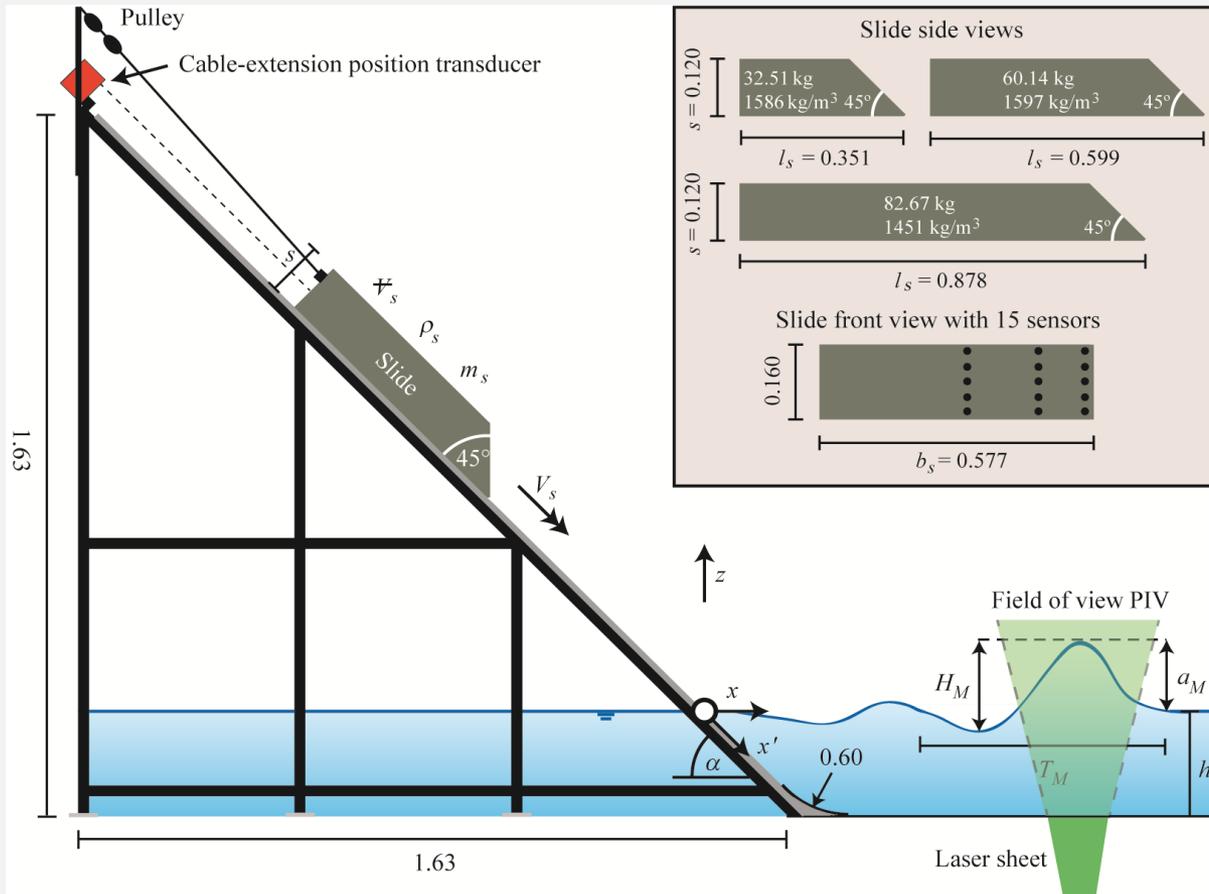


- Longitudinally slide impact
- Slide width \geq reservoir width (line source)
- Confined wave propagation along x

- Slide impact at any possible location
- Slide width $<$ reservoir width (point source)
- Free wave propagation on semi-circles along r and γ

Aims: Method to transform parameters from 2D to 3D and intermediate geometries

Models (physical)



Unknown parameters

- Maximum wave amplitude a_M
- Maximum wave height H_M
- Maximum wave period T_M

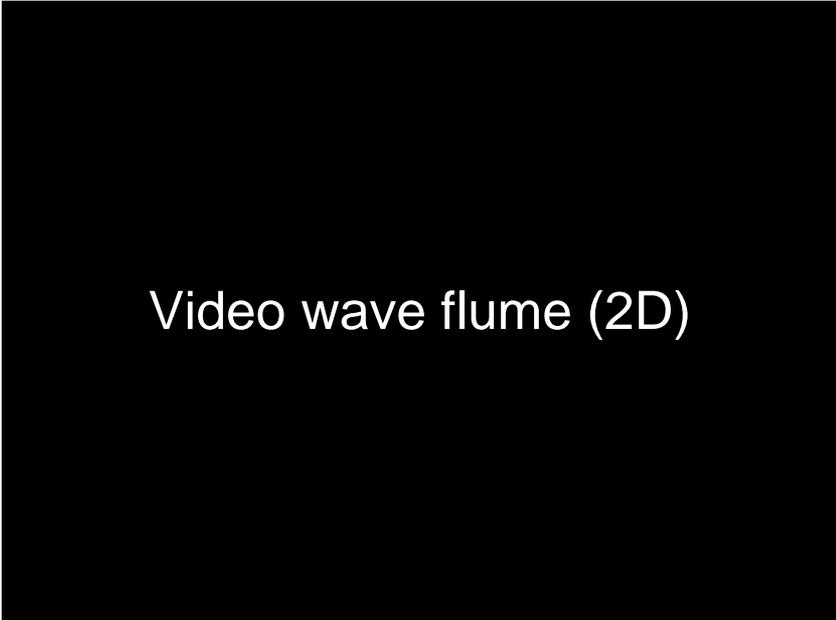
Known parameters

- Still water depth h (0.24 - 0.48 m)
- Slide mass m_s
- Slide impact velocity V_s (0.94 - 3.79 m/s)
- Slide volume V_s
- Slide thickness s
- Slide density ρ_s
- Slide impact angle α (45°)

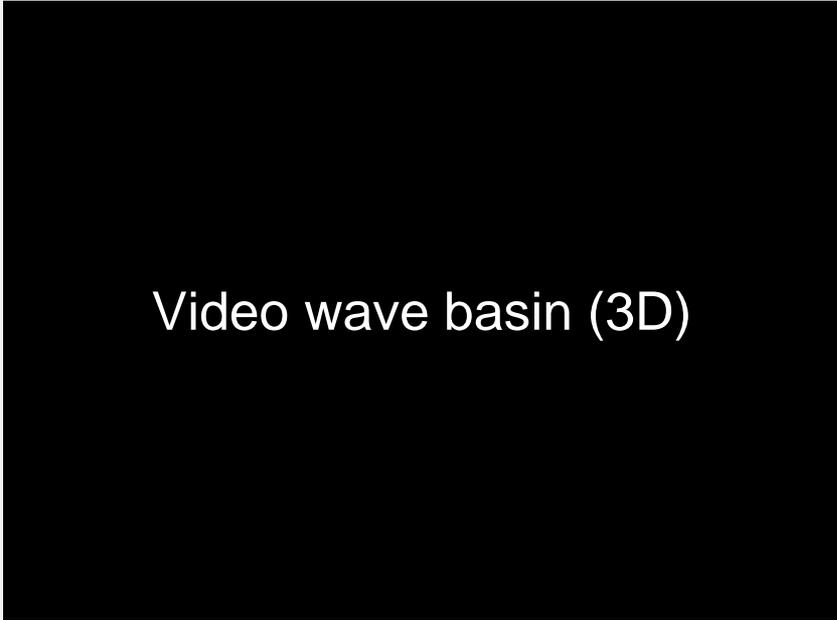


Models (physical)

Test in wave flume (unobstructed 21.0 m × 0.6 m) Test in wave basin (unobstructed 7.4 m × 20 m)



Video wave flume (2D)

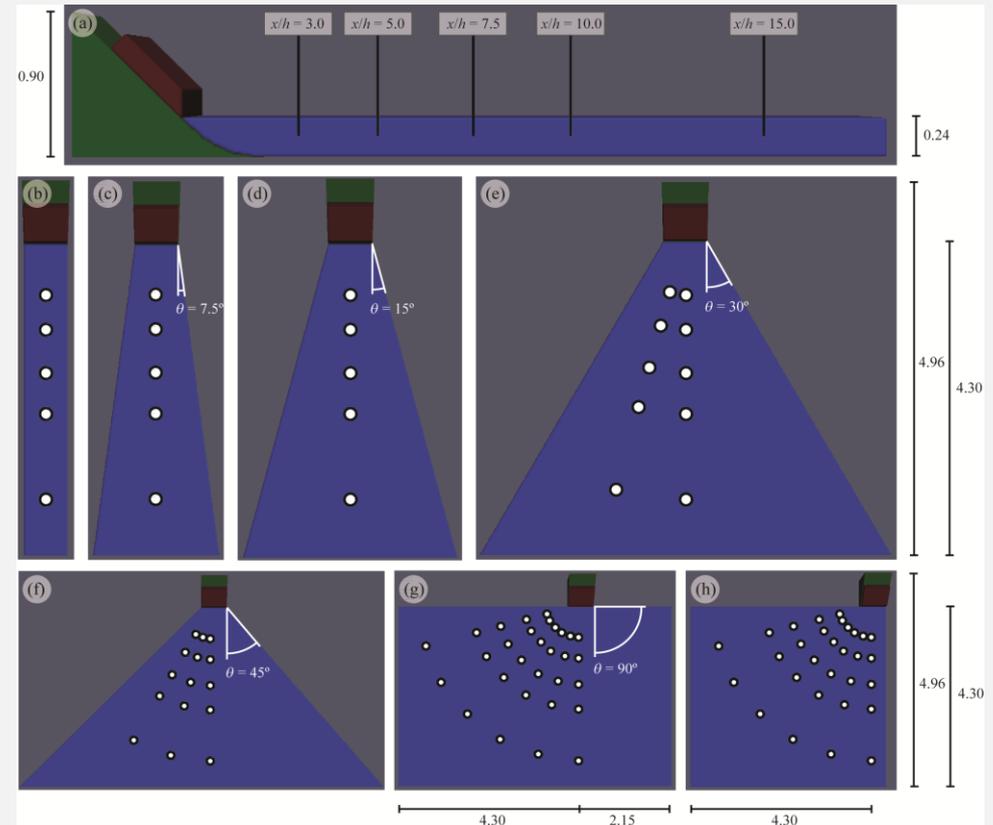


Video wave basin (3D)

- All conditions, apart from the water body geometry, are identical between 2D and 3D
- A total of 18 2D-3D test pairs were investigated involving different slide masses, release positions and wave types

Models (DualSPHysics)

- The **beta executable v3.1** was used
- v3.1 includes a **discrete element method (DEM)** formulation such that solid-solid and solid-fluid interaction may be simulated with contact law theory (Canelas et al. 2013)
- **DEM is essential** for the present work to model the slide as a floating object moving along a rigid-beach boundary
- A **bed friction coefficient**, Young's modulus and Poisson ratio can be specified in DEM
- **Formulations:** cubic spline kernel, artificial viscosity formulation, Verlet time-stepping algorithm, Delta-SPH density filter
- A **HPC clusters** was accessed (**12 core** Westmere nodes Intel® Xeon® CPU X5650 at 2.67 GHz with DDR3 memory running at 1333 MHz)
- Most expensive case herein ($dp = 10$ mm, 8 Mio particles) took **13 h per second** real time



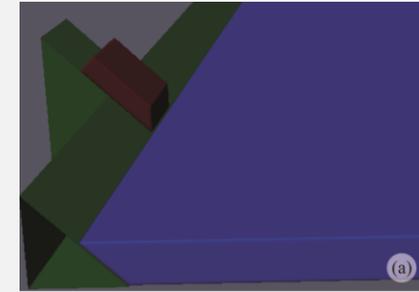
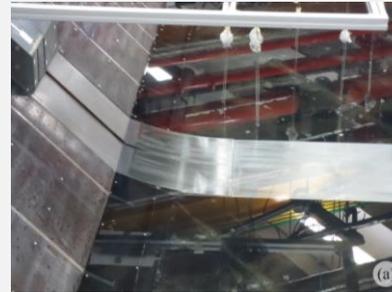
All geometries: (a,b) side and plane view of 2D case, (c) basin side angle $\theta = 7.5^\circ$, (d) 15° , (e) 30° , (f) 45° , (g) 90° (3D) and (h) 3D corner case 3Dc

Models (DualSPHysics)

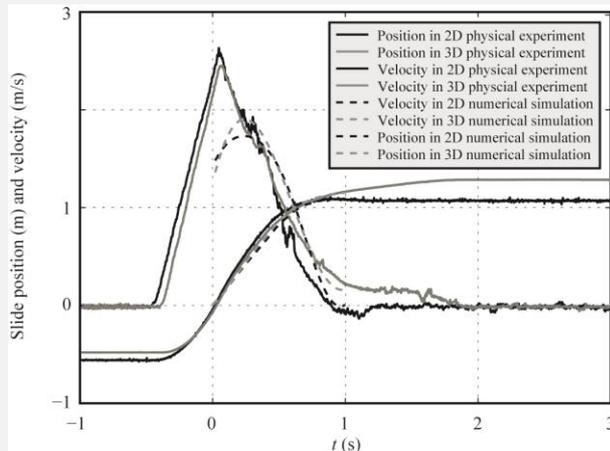
Validation and calibration of DualSPHysics

Numerical strategy:

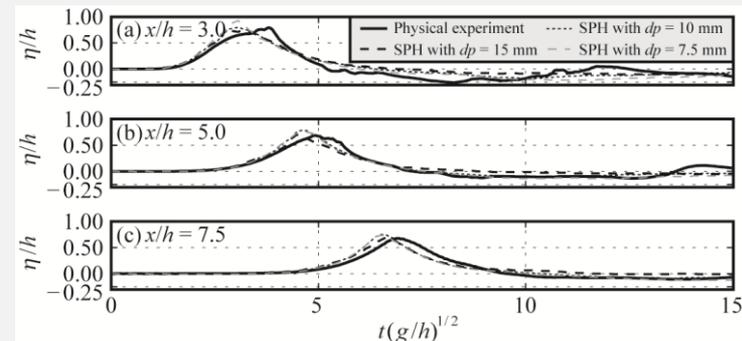
- Everything is identical to physical tests except that slide starts with slide nose at water surface
- The front impact velocity V_{sf} was adjusted to minimise the difference between $a_{M,Num}$ and $a_{M,Phys}$ ($V_{sf,Num} = 1.72 \text{ m/s} < V_{sf,Phys} = 2.43 \text{ m/s}$)



Slide positions and velocities



Convergence tests in 2D ($dp = 7.5, 10$ and 15 mm)

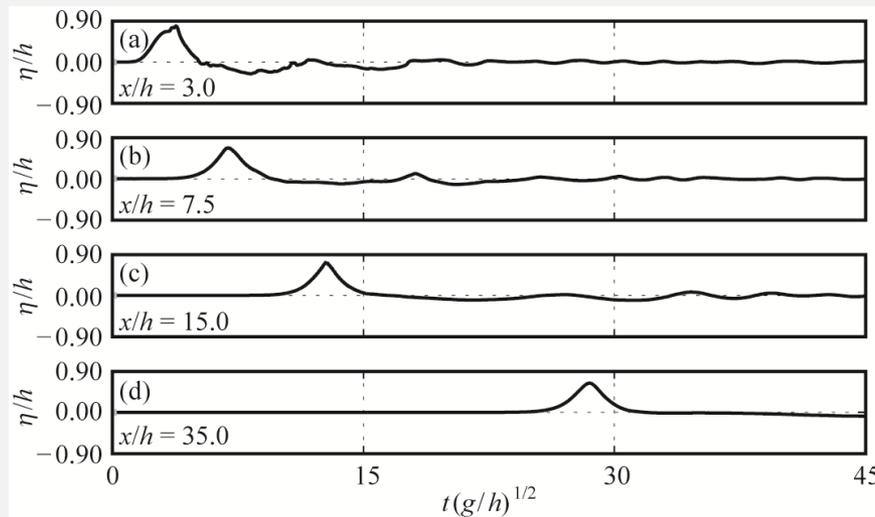


Convergence at $x/h = 5.0$ and 7.5 , unclear at $x/h = 3.0$ (non-linearities, multi-phase effects due to slide impact); $dp = 10 \text{ mm}$ seems an appropriate compromise between simulation time and accuracy

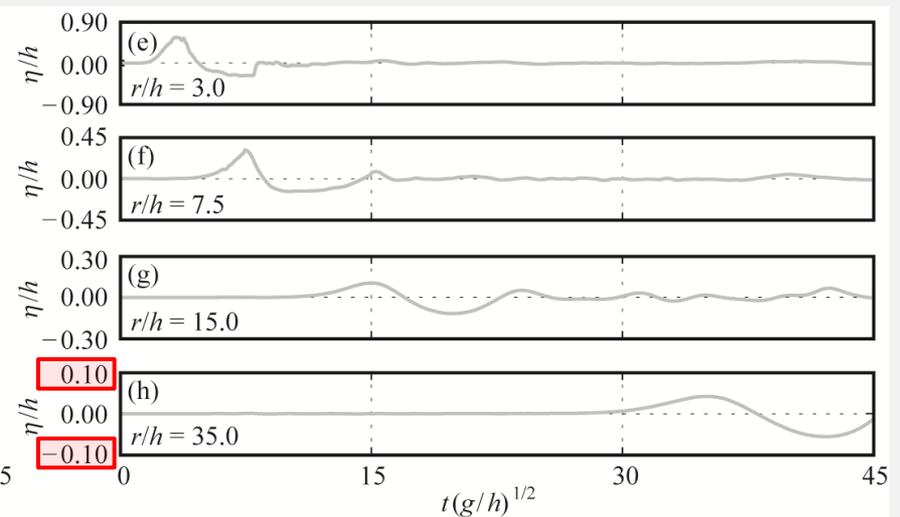
Results (physical)

Test conducted in 2D and 3D under otherwise identical BCs

2D: Wave flume geometry

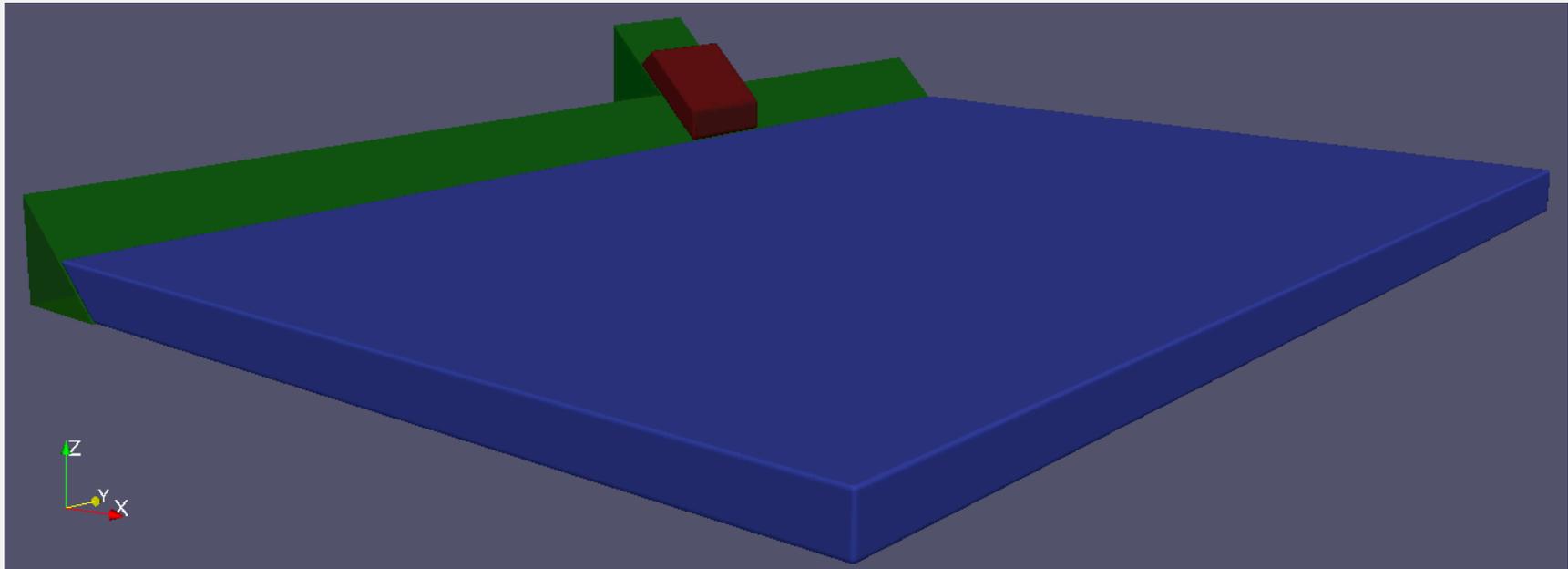


3D: Wave basin geometry



- In this case, the waves are only 30% different between 2D and 3D close to the slide impact zone
- Tsunami decays much faster in 3D, mainly due to spatial wave energy spread
- The wave amplitude in 3D is 16 times smaller than in 2D at $x/h = r/h = 35$

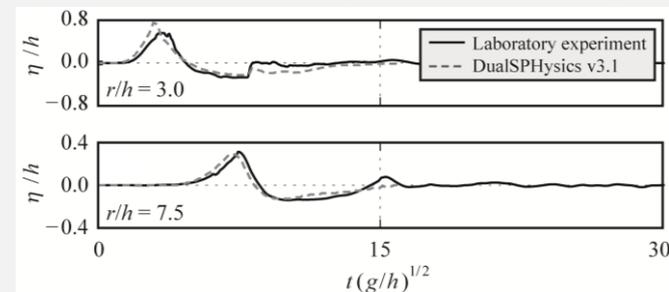
Results (DualSPHysics)



Numerical strategy:

- The 2D test (treated as a 3D problem) was used to calibrate DualSPHysics via V_{sf}
- The same value for V_{sf} as in 2D was then used for 3D
- The validation in 3D is shown on the right resulting in a good agreement with data from physical tests

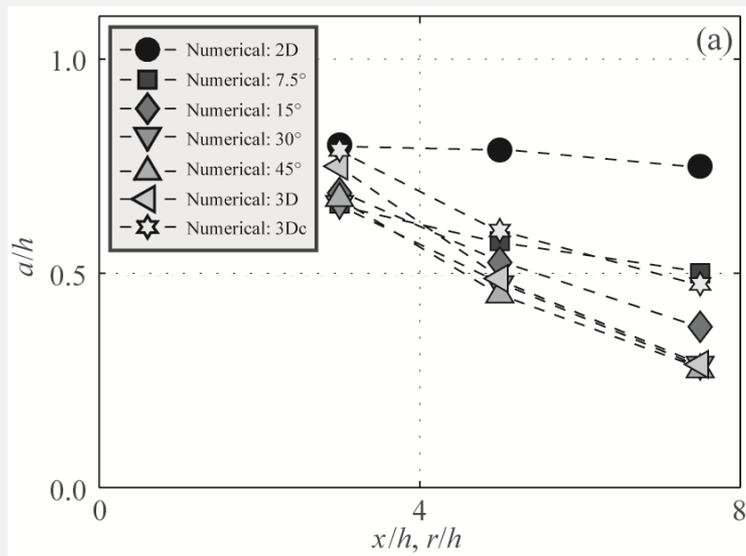
Physical and numerical wave profiles in 3D along slide axis



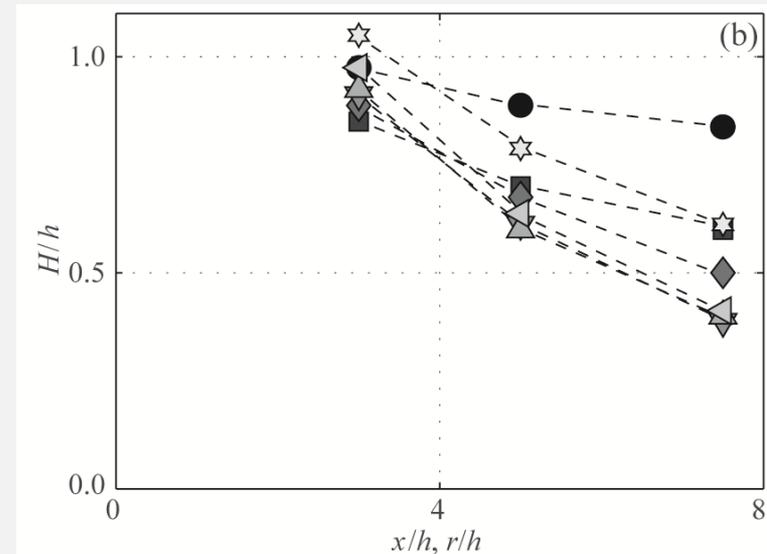
Results (DualSPHysics)

Investigation of intermediate geometries

Wave amplitude decay



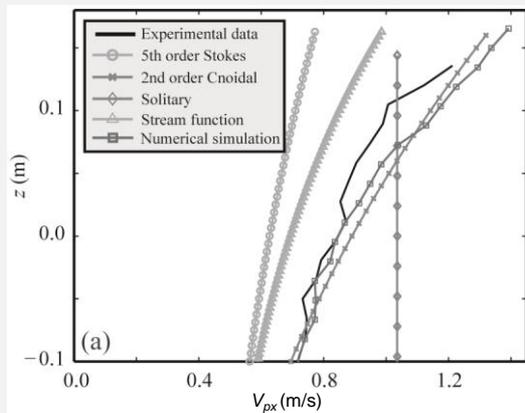
Wave height decay



- The wave parameters in the geometry with $\theta = 7.5^\circ$ lie approximately halfway between the values observed in 2D and 3D
- The wave parameters for $\theta \geq 30^\circ$ may be approximated with the 3D values

Results (physical, DualSPHysics and analytical kinematics)

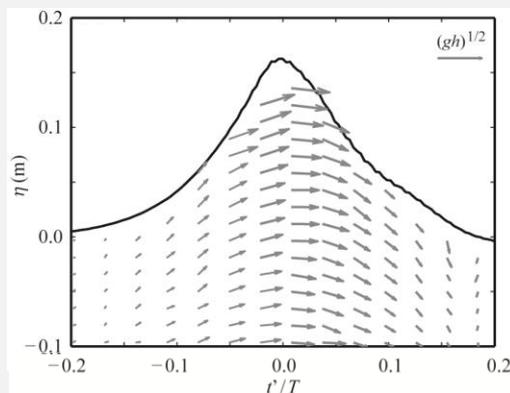
Wave crest kinematics (from SWL to crest) in 2D at $x/h = 7.5$



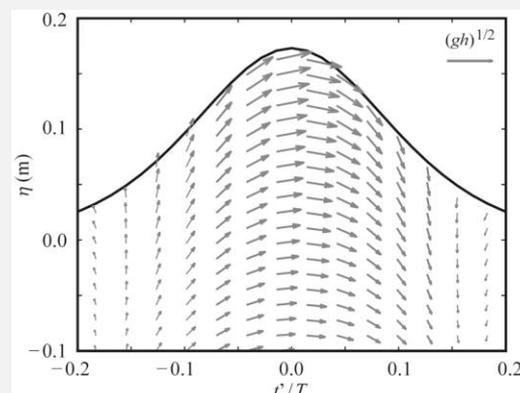
Method	Maximum v_{px} (m/s)	Mean v_{px} (m/s)
Measured	1.21	0.97
5 th order Stokes	0.77	0.69
2 nd order cnoidal	1.32	1.09
Solitary	1.04	1.04
Stream function	0.99	0.83
DualSPHysics	1.39	1.12

v_{px} = horizontal water particle velocity component

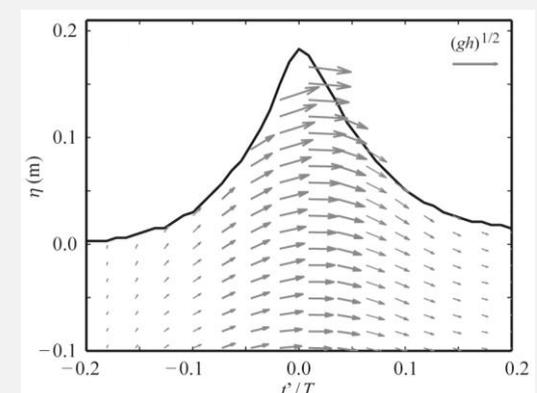
Measured (PIV)



Theoretical (cnoidal wave theory)



DualSPHysics



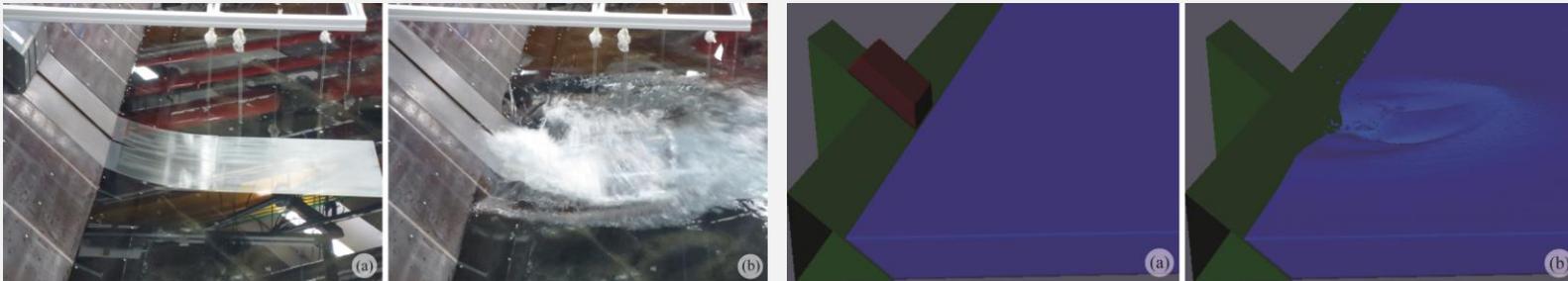


Conclusions

- The **effect of the water body geometry** on subaerial landslide-tsunamis (impulse waves) was investigated
- **Physical model tests** were conducted in a wave flume (2D) and basin (3D) and **numerical simulations** were carried out with DualSPHysics
- The geometrical effect is significant and deviations of **up to a factor of 16** between wave parameters in 2D and 3D were observed
- An overall **good agreement** between numerical and experimental results was achieved; DualSPHysics seems an **excellent option**
 - (i) to further investigate the effect of the water body geometry and
 - (ii) for case-specific landslide-tsunami hazard assessment (potential to be *the* leading code for such applications)
- Improvements in DEM (slide kinematics) and implementation of the Riemann solver would make DualSPHysics **even more promising** in this regard

Outlook

- Fully-funded PhD project to continue this research (get in touch)
- Ongoing and future tests are run with the GPU version of DualSPHysics
- Simulations of pressure on slide surface (physical model data available on SPHERIC website (validation test 11) and/or in Heller et al., 2015)



Acknowledgements

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Thank you for your attention!